

# New Optimization Tools: The Julia Computing Environment

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# Outline

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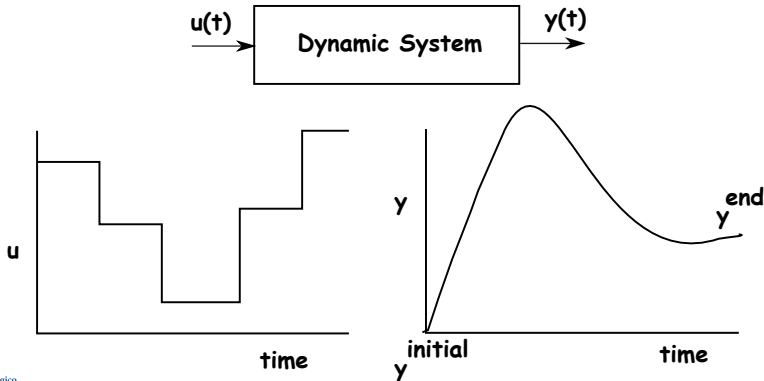
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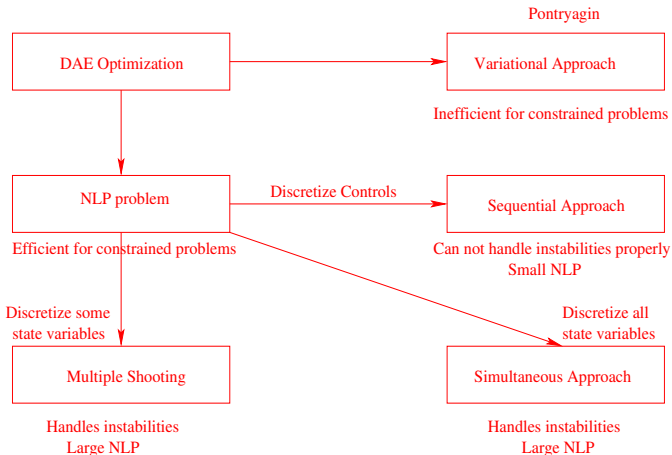
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## Traditional Optimal Model-based dynamic transitions

Take a dynamic system from an initial point to a final point in the best possible way



# Common Approaches for Solving Dynamic Optimization Problems





# Discretizing ODEs using Orthogonal Collocation

Given an ODE system:

$$\frac{dx}{dt} = f(x, u, p), \quad x(0) = x_{\text{init}}$$

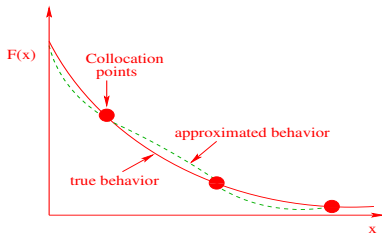
where  $x(t)$  are the system states,  $u(t)$  is the manipulated variable and  $p$  are the system parameters.

The aim is to approximate the behaviour of  $x$  and  $u$  by Lagrange interpolation polynomials (of orders  $\mathcal{K} + 1$  and  $\mathcal{K}$ , respectively) at collocation or discretization points  $t_k$ :

$$x_{k+1}(t) = \sum_{k=0}^{\mathcal{K}} x_k \ell_k^x(t), \quad \ell_k^x(t) = \prod_{\substack{j=0 \\ j \neq k}}^{\mathcal{K}} \frac{t - t_j}{t_k - t_j}$$

$$u_k(t) = \sum_{k=1}^{\mathcal{K}} u_k \ell_k^u(t), \quad \ell_k^u(t) = \prod_{\substack{j=1 \\ j \neq k}}^{\mathcal{K}} \frac{t - t_j}{t_k - t_j}$$

$$x_{N+1}(t_k) = x_k, \quad u_N(t_k) = u_k$$



Therefore replacing into the original ODE system, we get the system residual  $\mathcal{R}(t_k)$ :

$$\mathcal{R}(t_k) = \sum_{j=0}^{\mathcal{K}} x_j \frac{d\ell_j(t_k)}{dt} - f(x_k, u_k, p) = 0, \quad k = 1, \dots, \mathcal{K}$$

# Transformation of a Dynamic Optimization problem into a NLP

Original dynamic optimization problem

$$\min_{x, u} \phi(x, u)$$

$$\text{s.t.} \quad \frac{dx(t)}{dt} = F(x(t), u(t), t, p)$$

$$x(0) = x^0$$

$$g(x(t), u(t), p) \leq 0$$

$$h(x(t), u(t), p) = 0$$

$$x^l \leq x \leq x^u$$

$$u^l \leq u \leq u^u$$

Discretized NLP

$$\min_{x_k, u_k} \phi(x_k, u_k)$$

$$\text{s.t.} \quad \sum_{j=0}^{\mathcal{K}} x_j \dot{\ell}_j(t_k) - F(x_k, u_k) = 0, \quad k = 1, \dots, \mathcal{K}$$

$$x_0 = x(0)$$

$$g(x_k, u_k, p) \leq 0, \quad k = 1, \dots, \mathcal{K}$$

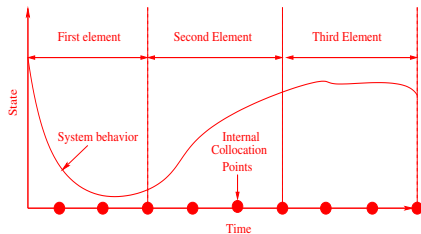
$$h(x_k, u_k, p) = 0, \quad k = 1, \dots, \mathcal{K}$$

$$x^l \leq x \leq x^u$$

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# Approximation of a Dynamic Optimization Problem using Orthogonal Collocation on Finite Elements

Sometimes it is convenient to use Orthogonal Collocation on Finite Elements to approximate the behavior of systems exhibiting fast dynamics.



$$\min_{x_k, u_k} \phi(x, u)$$

s.t.

$$\sum_{j=0}^{\mathcal{K}} x_{ij} \hat{\ell}_j(\tau_k) - h_i F(x_{ik}, u_{ik}) = 0, \quad i=1, \dots, NE, \quad k=1, \dots, NC$$

$$x_{10} = x(0)$$

$$g(x_{ik}, u_{ik}, p) = 0, \quad i = 1, \dots, NE; \quad k = 1, \dots, NC$$

$$x_{ij}^l \leq x_{ij} \leq x_{ij}^u, \quad i = 1, \dots, NE; \quad k = 1, \dots, NC$$

$$u_{ij}^l \leq u_{ij} \leq u_{ij}^u, \quad i = 1, \dots, NE; \quad k = 1, \dots, NC$$

where NE is the number of finite elements, NC is the number of internal collocation points,  $h_i$  is the length of each element.

# Example: Dynamic optimal transition between two steady-states: Hicks CSTR

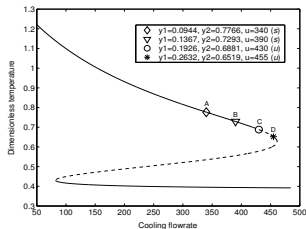
$$\frac{dC}{dt} = \frac{1 - C}{\theta} - k_{10}e^{-N/T}C$$

$$\frac{dT}{dt} = \frac{y_f - T}{\theta} + k_{10}e^{-N/T}C - \alpha U(T - y_c)$$

Parameter values

$\theta$	20	Residence time
$T_f$	300	Feed temperature
$J$	100	$(-\Delta H)/(\rho C_p)$
$k_{10}$	300	Preexponential factor
$c_f$	7.6	Feed concentration
$T_c$	290	Coolant temperature
$\alpha$	$1.95 \times 10^{-4}$	Heat transfer area
$N$	5	$E_1/(R J c_f)$

Desired Transition B  $\rightarrow$  A



Desired dynamic transition

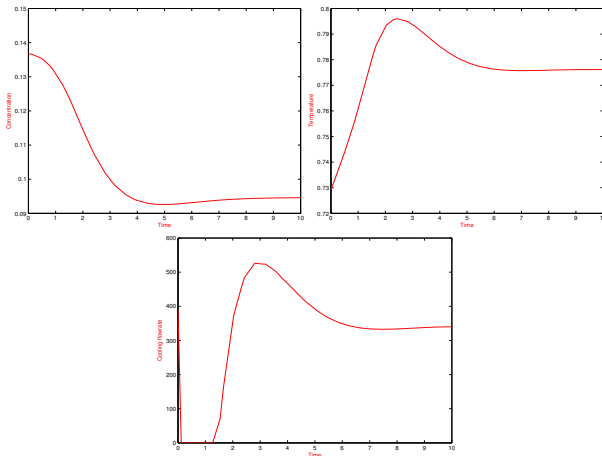
	C	T	U
Initial (B)	0.1367	0.7293	390
Final (A)	0.0944	0.7766	340

$C$  = Concentration ( $c/c_f$ ),  $T$  = temperature ( $T_r/Jc_f$ ),  $y_c$  = Coolant temperature ( $T_c/Jc_f$ ),  $y_f$  = feed temperature ( $T_f/Jc_f$ ),  $U$  = Cooling flowrate.  $c$  and  $T_r$  are nondimensionless concentration and reactor temperature.

# Dynamic Transitions profiles for the Hicks CSTR example

As objective function the requirement of minimum transition time between the initial and final steady-states will be imposed:

$$\text{Min} \int_0^{t_f} \left\{ \alpha_1 (C(t) - C_{\text{des}})^2 + \alpha_2 (T(t) - T_{\text{des}})^2 + \alpha_3 (U(t) - U_{\text{des}})^2 \right\} dt$$



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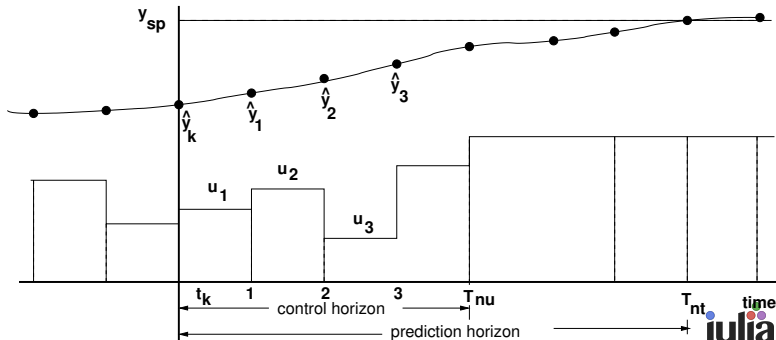
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- ▶ The aim of the last two terms is to penalize for large changes in both the states and manipulated variable values.

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- ▶ The aim of the last two terms is to penalize for large changes in both the states and manipulated variable values.

$$\Delta x_i = x_i - x_{i-1}$$

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In summary, the computation of optimal product dynamic transitions using a DFO approach can be cast as follows:

$$\min_{\mathbf{u}} \Omega = \sum_{i=1}^N [(x_i - x^f)^2 + (u_i - u^f)^2] + \lambda_x \sum_{i=1}^N [\Delta x_i]^2 + \lambda_u \sum_{i=1}^N [\Delta u_i]^2$$

$$\begin{aligned} \text{s.t.} \quad & x^l \leq x_i \leq x^u, & i = 1, \dots, N \\ & u^l \leq u_i \leq u^u, & i = 1, \dots, N \\ & \Delta x^l \leq \Delta x_i \leq \Delta x^u, & i = 1, \dots, N \\ & \Delta u^l \leq \Delta u_i \leq \Delta u^u, & i = 1, \dots, N \end{aligned}$$

where the  $l$  and  $u$  superscripts stand for lower and upper bounds, respectively.

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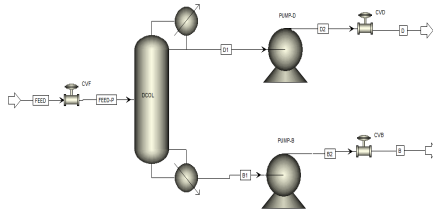
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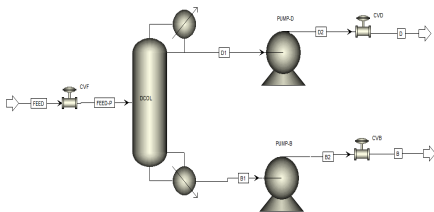
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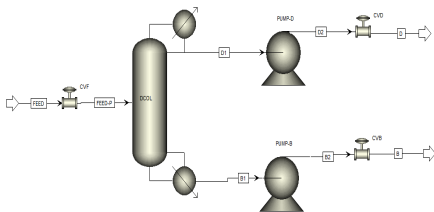
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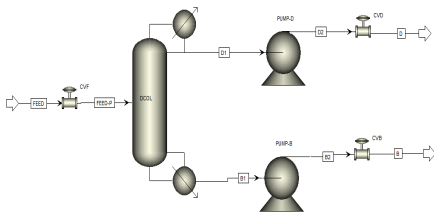
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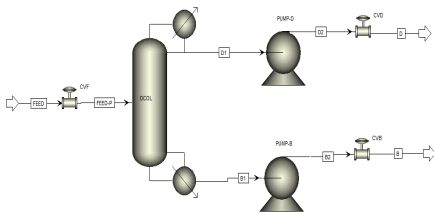
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- ▶ Objective function: we use a MPC formulation for the objective function.

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where  $c$  stands for the benzene mol fraction distillate stream which is the controlled variable,  $u$  stands for the reflux ratio which is the manipulated variable,  $N$  is the prediction and control horizons, the superscript  $d$  stands for desired or target values.

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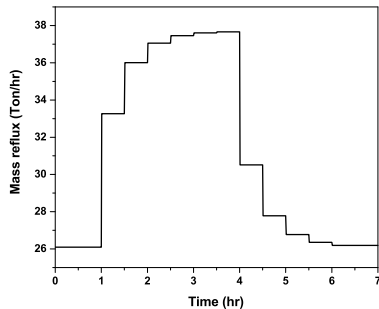
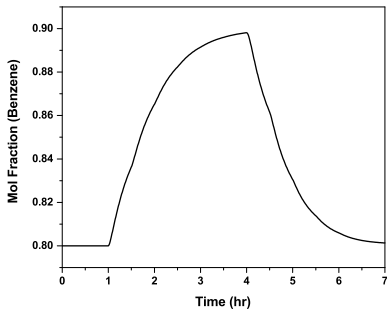
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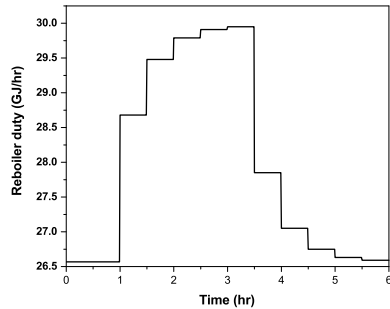
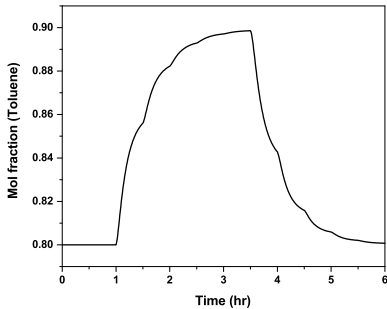
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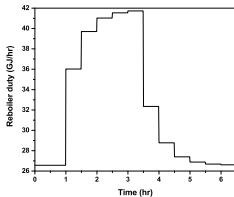
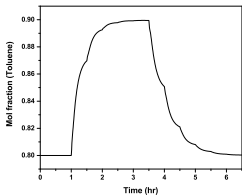
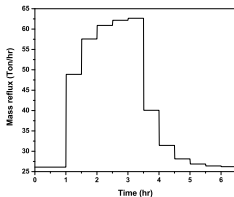
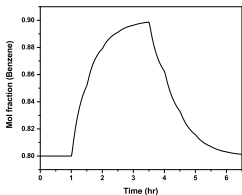


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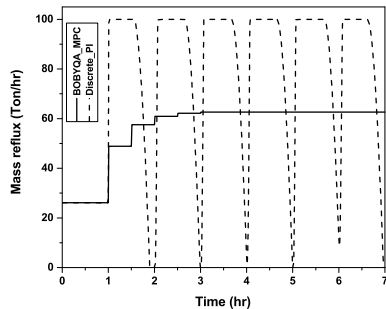
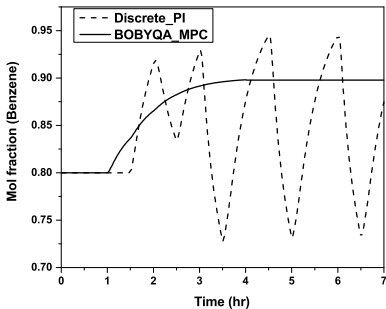




# Dual composition control of the distillate and bottoms streams



# Comparison against Proportional-Integral Controllers



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